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## Citation

Yuan, Junhua, Karen Aicia Fahrner, and Howard Curtis Berg. 2009. Switching of the bacterial flagellar motor near zero load. *Journal of Molecular Biology* 390(3): 394-400.

## Published Version

<http://dx.doi.org/10.1016/j.jmb.2009.05.039>; doi:10.1016/j.jmb.2009.05.039

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# **Switching of the bacterial flagellar motor near zero load**

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## **Abstract**

**Flagellated bacteria, such as *Escherichia coli*, are able to swim up gradients of chemical attractants by modulating the direction of rotation of their flagellar motors, which spin alternately clockwise (CW) and counterclockwise (CCW). Chemotactic behavior has been studied under a variety of conditions, mostly at high loads (at large motor torques). Here, we examine motor switching at low loads. Nano-gold spheres of various sizes were attached to hooks (the flexible coupling at the base of the flagellar filament) of cells lacking flagellar filaments in media containing different concentrations of the viscous agent Ficoll. The speeds and directions of rotation of the spheres were measured. Contrary to the case at high loads, motor switching rates increased appreciably with load. Both the CW→CCW and CCW→CW switching rates increased linearly with motor torque. Evidently, the switch senses stator-rotor interactions as well as the CheY-P concentration.**

*Keywords: Escherichia coli; nano-gold; torque; speed; allostery.*

## Introduction

Cells of *Escherichia coli* are propelled by several helical flagellar filaments, each driven at its base by a reversible rotary motor. When all the motors on a cell turn counterclockwise (CCW), the filaments coalesce into a helical bundle that pushes the cell steadily forward (in a run). When one or more motors switch to clockwise (CW), their filaments come out of the bundle and go through a series of polymorphic transformations (changes in handedness and shape) that result in uncoordinated movement (a tumble) and choice of a new direction for another run<sup>1</sup>. Tumbles are suppressed when cells move up spatial gradients of chemical attractants<sup>2</sup>. Thus, by controlling the direction of rotation of their flagellar motors, cells are able to move toward regions that are more favorable.

Torque is thought to be generated by electrostatic interactions between the stator protein MotA and the rotor protein FliG, resulting from conformational changes in MotA and MotB (another stator protein), driven by protonation and deprotonation of MotB Asp32<sup>3; 4</sup>. The energy for this process is derived from the change in the electrochemical potential of a proton as it moves from the outside to the inside of the cell. The direction of rotation (switching) is controlled by interaction of the cytoplasmic response regulator CheY-P with the rotor protein FliM<sup>5; 6; 7</sup>. Torque generation and switching have been modeled separately: for torque generation, see<sup>8; 9</sup>; for switching, see<sup>10; 11; 12</sup>.

In earlier work at intermediate and high loads, we found that CW→CCW switching rates decreased with motor torque, most notably in the speed range between 50 Hz and stall, while CCW→CW switching rates remained more nearly constant, with the result that the motor became more CW biased at lower speeds<sup>13</sup>. The highest speeds (~200 Hz at room temperature) were observed with 0.36  $\mu\text{m}$  diameter latex beads

attached to filament stubs. Recently, we developed an assay that allowed study of the motor near zero load, in which 60-nm diameter gold spheres were attached to hooks of cells lacking flagellar filaments<sup>14</sup>. A dark-field image of such a sphere, observed through a small pinhole, wobbles as the sphere rotates, generating an oscillating signal whose frequency is readily measured (~330 Hz at room temperature). In the present work, by using two orthogonal slits and a second detector, we monitored the direction of rotation as well as the speed. We used gold spheres of different sizes in motility medium containing different concentrations of Ficoll, estimating motor torque from the product of speed times rotational viscous drag coefficient. We found that near zero load both the CW→CCW and CCW→CW switching rates increased linearly with motor torque, with motor bias remaining constant. The data could be fit by the model of Duke, LeNovère, & Bray<sup>11</sup> in which the activities of a ring of proteins change by conformational spread, assuming that the rates for transitions between active and inactive states of individual subunits are torque-dependent.

## Results

Gold spheres coated with anti-hook antibody were attached to hooks of cells stuck to a polylysine-treated glass coverslip. Light scattered from a sphere was focused on two orthogonal slits in front of two photomultiplier tubes, as shown schematically in Fig. 1, generating  $x$  and  $y$  signals of the sort shown in Fig. 2. These signals, plotted separately (A, B) or in polar coordinates (C), allowed us to measure rotation rates as a function of time (D). Velocity time series were converted into binary time series, from which CW and CCW intervals were extracted.

We studied the switching statistics of the motor at near-zero to low loads, using spheres of diameters 100, 150, or 200 nm in motility medium, or spheres of diameter 200 nm in motility medium containing Ficoll at 5%, 10%, or 15% w/v. The mean CW and CCW intervals were determined for each motor at a specified torque, as shown in Fig. 3. The median and interquartile range of the intervals for each load were calculated and are shown in Fig. 4 A and B, which include data for intermediate loads from ref.<sup>13</sup> (for the three lowest loads using 0.36, 0.54, and 0.75- $\mu$ m diameter beads on filament stubs in motility medium). Both CW and CCW intervals decreased dramatically with load, with the ensemble median decreasing from  $\sim 0.8$  to 0.2 s and from  $\sim 4$  to 1 s for CW and CCW intervals respectively. The corresponding switching rates are shown in Fig. 4 C and D, with  $k_{\text{CW} \rightarrow \text{CCW}} = 1/\langle \text{CW} \rangle$  and  $k_{\text{CCW} \rightarrow \text{CW}} = 1/\langle \text{CCW} \rangle$ , where  $\langle \text{CW} \rangle$  and  $\langle \text{CCW} \rangle$  are ensemble medians of CW and CCW intervals respectively. Both switching rates increased with motor torque, with a dependence that was approximately linear.

We were concerned that the Ficoll used in our experiments might contain a hydrolysis product (glucose, a chemoattractant) that would perturb the switching statistics, so we did additional measurements with gold spheres of diameter 150 nm in 5% Ficoll. In this case, the viscous drag is nearly the same as for spheres of diameter 200 nm in motility medium. As can be seen in Fig. 5 A, B and C, the CW and CCW intervals and CCW biases were essentially the same.

The data of Fig. 4 are plotted again in Fig. 6 as a function of CCW speed. The switching rates decreased with speed, as expected, given that motor torque is known to fall linearly in the low-torque, high-speed regime from a plateau ending at  $\sim 160$  Hz to 0 at  $\sim 330$  Hz<sup>15; 16</sup>. A plot of this part of the torque-speed relationship is shown in Fig. 7.

## Discussion

The flagellar motor has a distinctive torque-speed relationship. At room temperature, torque is maximum at stall, it falls ~10% between 0 and ~160 Hz, and then, as just noted, it drops rapidly, reaching 0 at ~330 Hz<sup>15</sup>. In the high-torque, low-speed regime, torque is independent of temperature, and solvent isotope effects are relatively small; in the low-torque, high-speed regime, torque increases with temperature, and solvent isotope effects are large<sup>17</sup>. Evidently, at low speeds, rates of displacement of internal mechanical components or of translocation of protons are not limiting, whereas at high speeds, they are limiting. Comparison of our earlier results<sup>13</sup> with those obtained here show that the switching behavior also is different in these two regimes, Fig. 8. In the high-torque, low-speed regime, the switching rates increase with speed, the CW→CCW rates more rapidly than the CCW→CW rates, thus increasing the CCW motor bias. In the low-torque, high-speed regime, the switching rates decrease with speed to an equivalent degree, without changing the motor bias. In the discussion that follows, we will attempt to understand the behavior near zero torque in terms of the mechanism for switching proposed by Duke et al.<sup>11</sup>. We do not yet understand the behavior at high torques.

Switching is commonly described by a thermal isomerization model, in which CW and CCW states are separated by an energy barrier<sup>18</sup>. The switching rates between these states are proportional to  $\exp(-\Delta G^\ddagger/kT)$ , where the activation energy  $\Delta G^\ddagger$  is the difference between the free energy of the barrier and that of either the CW or CCW state. An increase in CheY-P binding lowers the free energy of the CW state and raises the free energy of the CCW state<sup>12</sup>, so that the CW→CCW and CCW→CW switching rates

change in a reciprocal manner. According to our measurements near zero torque, both switching rates ( $k_{\text{CW} \rightarrow \text{CCW}}$  and  $k_{\text{CCW} \rightarrow \text{CW}}$ ) increase with torque by the same factor (a factor of about 4 for torques from 0 to 1300 pN nm). This suggests a refinement in which the activation energies of the CW and CCW states are lowered by a stator-rotor interaction. If the magnitude of this change in free energy were of order  $\tau\theta$ , where  $\tau$  is the motor torque and  $\theta$  is the angular change in orientation of FliG (in a rotor-fixed coordinate system) that occurs when the motor switches, then one would expect an exponential increase in switching rate with torque, as predicted by a recent model of switching dynamics<sup>19</sup>. Instead, we observed switching rates that were linear with torque, so we sought a different explanation.

Consider the allosteric model proposed by Duke et al.<sup>11</sup>, in which a switching event is mediated by conformational changes in a ring of subunits that spread from subunit to subunit via nearest-neighbor interactions. Each subunit exists in either an inactive or active state, states that promote CCW or CW rotation, respectively. The free energy of the active state relative to that of the inactive state changes from  $+E_A$  to  $-E_A$  when a subunit binds ligand (CheY-P); ligand binding favors the active state. The coupling energy between adjacent subunits is  $-E_J$  if they are in the same state but zero otherwise; this favors like conformations. Switching from the fully inactive (CCW) to the fully active (CW) configuration occurs in two steps. First, a subunit undergoes a conformational change to nucleate an active domain. Then, this domain grows until it spreads throughout the entire ring. The nucleation occurs at a rate  $N\omega\exp(-\Delta E/kT)$ , where  $N=34$  is the number of subunits in the ring,  $\omega$  is the rate of conformational transition in either direction for each subunit, and  $\Delta E=2E_J-E_A$  (or  $2E_J+E_A$ ) depending upon whether



or not a ligand is bound to the subunit<sup>11</sup>. The probability that the domain grows from size 1 to size  $N$  without shrinking to zero is limited by the ligand binding rate,  $k_{\text{ligand}}$ . Because of different binding constants for active and inactive subunits, an active domain nucleated by chance will remain energetically disfavored until it is stabilized by ligand binding. If the subunit transition frequency is increased by a factor  $\exp(\tau\theta/kT)$ , the active subunit will have less time to wait for ligand binding before it transits back to the inactive conformation, thereby decreasing the probability that the nucleation event leads to switching. Therefore, the effect of the stator-rotor interaction on rates of switching will be less than exponential.

To determine the exact dependence of switching rates on motor torque, we performed Monte-Carlo simulations of the Duke et al. model, and the results are shown in Fig. 9 A and B. The switching rates increased nearly linearly with torque before reaching a plateau, where the plateau was due to the limitation of the ligand binding rate. To obtain a factor of about 4 increase before reaching the plateau, we set the value of  $k_{\text{ligand}}$  to be  $30 \text{ s}^{-1}$ , larger than assumed in ref.<sup>11</sup> ( $10 \text{ s}^{-1}$ ), but close to the value measured in ref.<sup>6</sup> ( $\sim 20 \text{ s}^{-1}$ ). All other parameters were similar to those of ref.<sup>11</sup>:  $E_A = 1 \text{ kT}$ ,  $E_J = 4 \text{ kT}$ ,  $\omega = 0.5 \times 10^4$  and  $E_L$  (the decrease in free energy of a subunit upon binding the ligand CheY-P)  $= -0.085 \text{ kT}$ , giving the wild-type CCW bias of about 80%. We fit the simulation curves (Fig. 9 A, B) to our data using two free parameters,  $\theta$  and a scaling factor for the vertical axis (for the switching rates). We could fit both sets of data with  $\theta/kT = 3.3 \times 10^{-3} \text{ (pN nm)}^{-1}$ , corresponding to  $\theta = 0.8^\circ$  (Fig. 9 C, D). Thus, our results are consistent with the allosteric model proposed by Duke et al. We note that there must be variations in the orientations of different FliG molecules depending upon stator-rotor interactions, so that

$0.8^\circ$  is some appropriately-weighted average value, with  $\tau\theta$  the average amount of work performed by the stator on the rotor to promote switching.

## **Materials and Methods**

### **Bacteria and cultures**

*E. coli* strain KAF83 was used to monitor wild-type motors. It is a derivative of AW405<sup>20</sup> carrying null mutations in *pilA* and *fliC*, but otherwise wild type for motility and chemotaxis. Cells were grown at 33°C in T-broth (1% tryptone, 0.5% NaCl) supplemented with the appropriate antibiotics to OD<sub>600</sub> ~0.5.

### **Sample preparation**

Cells were washed twice by centrifugation at 3000×g, and resuspended in motility medium (10 mM potassium phosphate, 0.1 mM EDTA, 10 mM lactate, 70mM NaCl, pH 7.0). Gold spheres of diameter 100, 150, or 200 nm (15711, 15712, 15713, Ted Pella Inc.) were attached to the hooks of KAF83 cells with anti-hook antibody, following the procedure described in ref.<sup>14</sup>. A sample was placed on a glass coverslip coated with poly-L-lysine (P4707, Sigma) and allowed to stand for 5 min. The coverslip was installed as the top window of a flow cell<sup>21</sup> and rinsed with motility medium. A 30% w/v stock solution of Ficoll 400 (dialyzed and lyophilized, 46324, Sigma) was prepared in motility medium, and other concentrations (5%, 10%, and 15% w/v) were made from this stock solution by dilution with motility medium.

### **Laser dark-field microscopy**

The apparatus is shown in Fig. 1. It was modified from that of ref.<sup>14</sup> by addition of a 50/50 beam splitter, two 3×1 mm precision slits (NT39-908, Edmund Optics) mounted at

right angles to one another, and a second photomultiplier tube (identical to the first).

Slit1 gave the  $x$  position information, while slit2 gave the  $y$  information. When the center of rotation of the image of a gold sphere was aligned at one of the corners of the intersection of the slits, the phases of the signals from the two photomultiplier tubes differed by 90 or -90 degrees, depending upon the direction of rotation, as shown in Fig.

2.

### **Experimental procedure**

The microscope stage was moved to align the center of rotation of the image of a gold sphere to a corner of the slit intersection, as described above. Data were accumulated for a period of 3 min for each motor, for 3 different sizes of gold spheres, 100, 150, and 200 nm in 0% Ficoll, and for 200 nm gold spheres in 3 different concentrations of Ficoll, 5%, 10% and 15%. Solutions were exchanged (drawn through the flow cell) at a rate of 70  $\mu\text{l}/\text{min}$ . When working with Ficoll, 7 min was allowed to ensure that the flow cell reached equilibrium. In all cases, the flow was continued throughout the experiment. All experiments were performed at room temperature (23°C).

### **Data analysis**

The anode currents from the two photomultiplier tubes were converted to voltages, which were DC-coupled to two 8-pole low-pass Bessel filters (3384, Krohn-Hite) with a cut-off frequency of 700 Hz. The filter outputs were sampled at 3 KHz by a computer data-acquisition system controlled by LabVIEW (National Instruments, Austin, TX). Offline data analysis was done by using custom scripts in MATLAB (MathWorks, Natick, MA). The  $x$  and  $y$  signals (approximating cosine and sine functions) were scaled so that the peak values ranged from -1 to +1, and then converted to polar coordinates. The angle

was differentiated with respect to time to yield the rotation rate (CW positive and CCW negative), and the output was smoothed with a 40-point running average. Switching was determined with a two-threshold-crossing algorithm: for each 3-min measurement, the speed histogram was plotted, and the peak positions at positive and negative velocities were extracted, corresponding to the steady-state CW and CCW rotation rates,  $v^+$  and  $v^-$ . The span between these values,  $(v^+ - v^-)$ , was divided by three to give three intervals. Switching from CW to CCW was flagged when the velocity crossed from the top interval to the bottom interval, and switching from CCW to CW was flagged when the velocity crossed from the bottom interval to the top interval. The time resolution was about 10 ms, limited mostly by the 40-point running average.

Torque was calculated from the rotational frictional drag coefficient multiplied by the angular velocity. For a gold sphere on a hook, neglecting the contribution of the hook, the drag coefficient is  $8\pi\eta a^3 + 6\pi\eta al^2$ , where  $a$  is the radius of the sphere,  $\eta$  is the viscosity of the medium, and  $l$  is the rotational eccentricity, i.e., the distance between the rotational axis and the center of the sphere. The drag coefficient ranges from  $8\pi\eta a^3$  to  $14\pi\eta a^3$  for  $l$  ranging from 0 to  $a$ . The average value  $11\pi\eta a^3$  was chosen with an estimated error of 20%. The values of viscosity for various concentrations of Ficoll were obtained from ref.<sup>15</sup>. For a latex bead on a filament stub, i.e., for the data from ref.<sup>13</sup>, the drag is the sum of contributions from the rotation of the bead and the filament stub. Calculation of the drag coefficient in this case was done as in refs.<sup>22; 23</sup>, assuming a bead rotational eccentricity of 0.2  $\mu\text{m}$  and a filament stub length of 1  $\mu\text{m}$ . The error was estimated to be 10%, resulting from uncertainties in eccentricity, stub length, and bead radius.

## **Acknowledgements**

We thank T.S. Shimizu and Y. Tu for helpful discussions. This work was supported by National Institutes of Health Grant AI016478.

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## Figure legends

**Fig. 1.** Schematic view of the apparatus: 655nm laser light scattered by a gold sphere was sampled by a 50/50 beam splitter, focused onto two 3×1 mm slits mounted at right angles to one another, and collected by a photomultiplier tube (PMT) behind each slit. The truncated 60° prism and the long-working-distance phase-contrast condenser allowed cells to be observed by phase contrast.

**Fig. 2.** (A)  $x$  signal (PMT1) as a function of time. (B)  $y$  signal (PMT2) as a function of time. (C) a plot of  $y$  versus  $x$ , showing the trajectory of the image of the gold sphere. (D) a sample trace showing switching: rotation rate of the sphere as a function of time. ‘-’: counter-clockwise. ‘+’: clockwise. The signals are voltages proportional to the PMT output currents.

**Fig. 3.** (A) Mean CW intervals, and (B) mean CCW intervals, plotted as a function of motor torque. The symbols are values for each cell. Reading from left to right, the load conditions were 100, 150 or 200-nm diameter gold spheres in motility medium, and 200-nm diameter gold spheres in 5%, 10%, or 15% Ficoll. The number of cells studied at each of these load conditions were 29, 45, 19, 15, 15, and 15, respectively.

**Fig. 4.** Median and interquartile range for (A) CW intervals and (B) CCW intervals, plotted as a function of motor torque. The corresponding rate constants  $k_{\text{CW-CCW}} = 1/\langle \text{CW} \rangle$  and  $k_{\text{CCW-CW}} = 1/\langle \text{CCW} \rangle$  are plotted in (C) and (D), along with linear fits. Open circles are results from this study, while open squares are results from ref.<sup>13</sup>.

**Fig. 5.** (A) Mean CW intervals, (B) mean CCW intervals, and (C) CCW biases, under two conditions with equivalent loads: (left) gold spheres of diameter 150 nm in 5% Ficoll; (right) gold spheres of diameter 200 nm in motility medium. Note that the motor torques in these two cases were nearly the same: the horizontal scale is expanded. The closed dots are values for each cell, and the open circles are means for each load condition. The number of cells studied on the left was 17, and on the right 15.

**Fig. 6.** Median and interquartile range for (A) CW intervals and (B) CCW intervals, plotted as a function of CCW speed. The corresponding rate constants  $k_{\text{CW-CCW}} = 1/\langle \text{CW} \rangle$  and  $k_{\text{CCW-CW}} = 1/\langle \text{CCW} \rangle$  are plotted in (C) and (D), along with linear fits. Open circles are results from this study, while open squares are results from ref.<sup>13</sup>.

**Fig. 7.** Mean torque as a function of mean CCW speed, along with a linear fit. Open circles are results from this study, while open squares are results from ref.<sup>13</sup>.

**Fig. 8.** The rate constants  $k_{\text{CW-CCW}} = 1/\langle \text{CW} \rangle$  and  $k_{\text{CCW-CW}} = 1/\langle \text{CCW} \rangle$  plotted as a function of CCW speed, along with linear fits. Note the extension of the speed axis to 0 Hz. Open circles are results from this study, while open squares are results from ref.<sup>13</sup>.

**Fig. 9.** (A, B) Monte-Carlo simulations of the model of Duke et al.<sup>11</sup>. Each data point is the mean and standard deviation of 8 independent simulations, and each simulation is a 500 s long switching trace. (C, D) Fitting of the simulation to the measurements, with

two free parameters in each fit:  $\theta$  and a scaling factor in the vertical axis. Symbols with error bars are the measurements, and lines are the fitting of simulations.

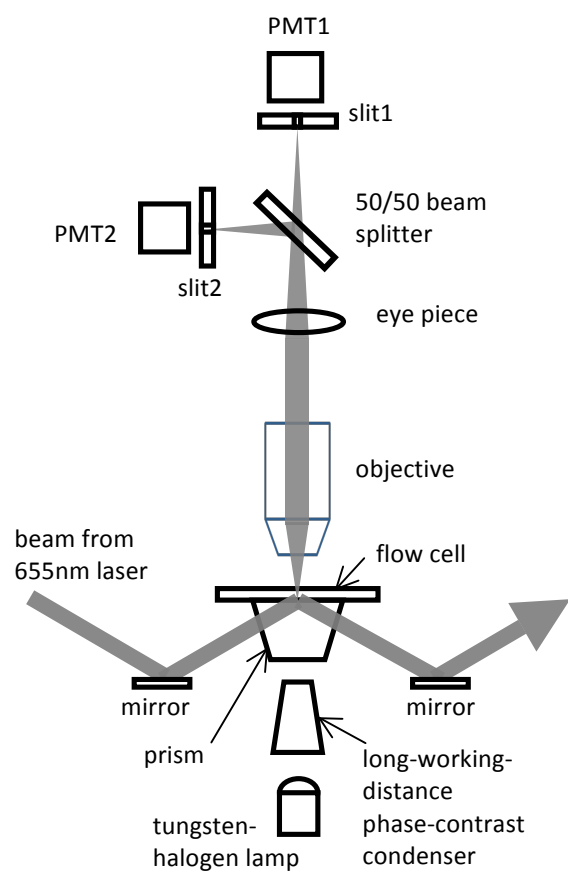


Fig. 1

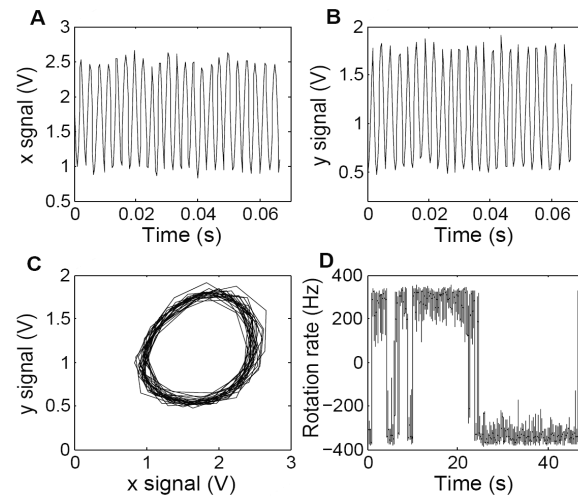


Fig. 2

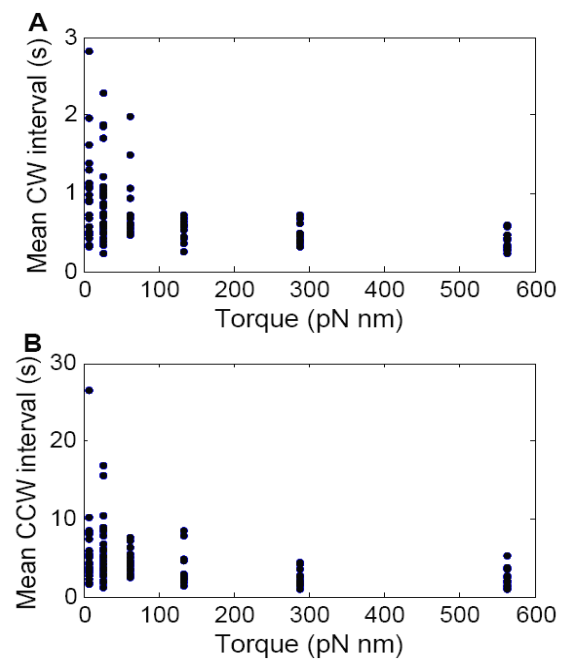


Fig. 3

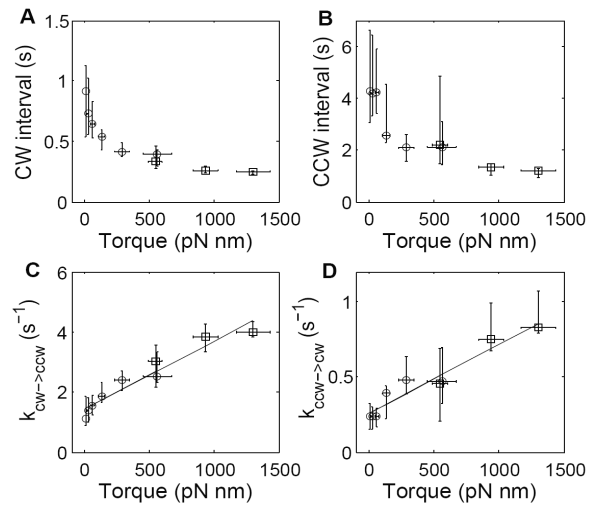


Fig. 4

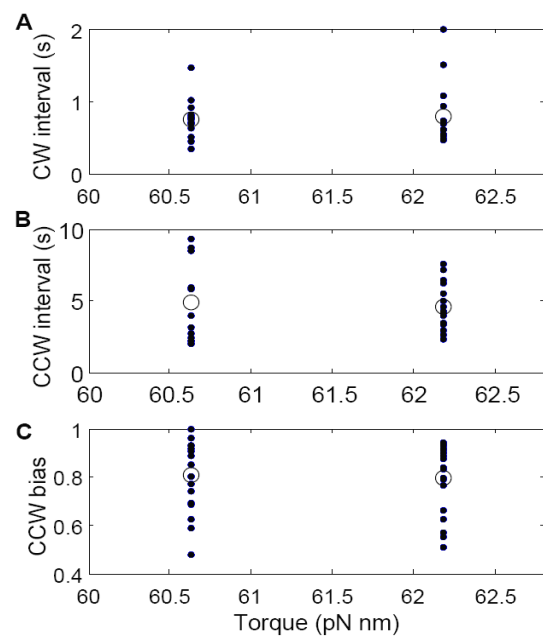


Fig. 5



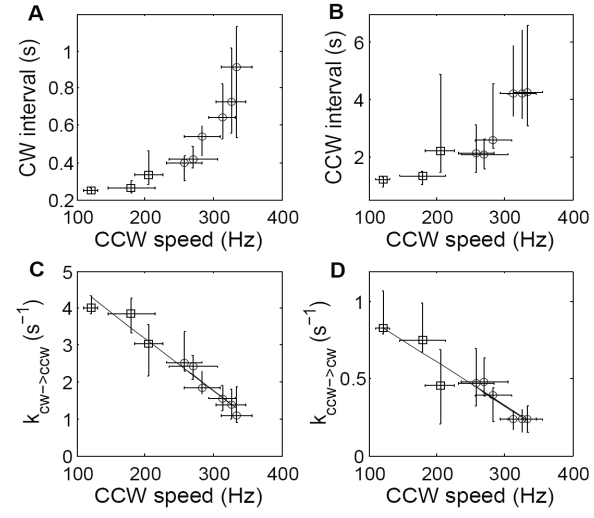


Fig. 6

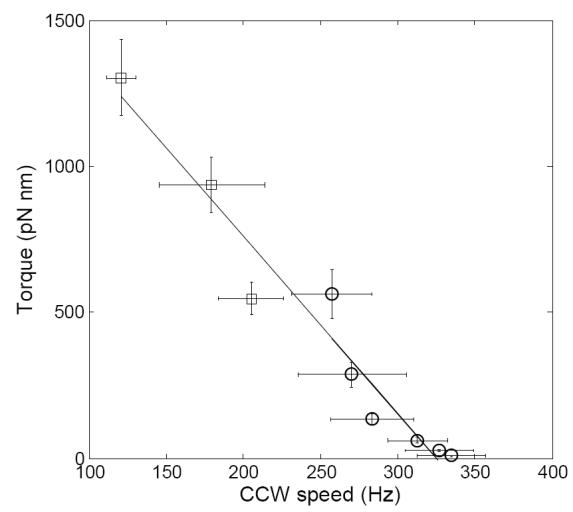


Fig. 7

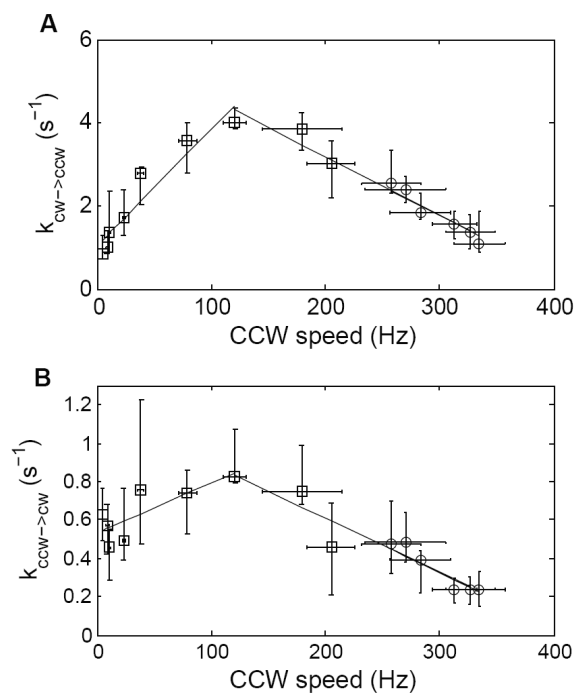


Fig. 8

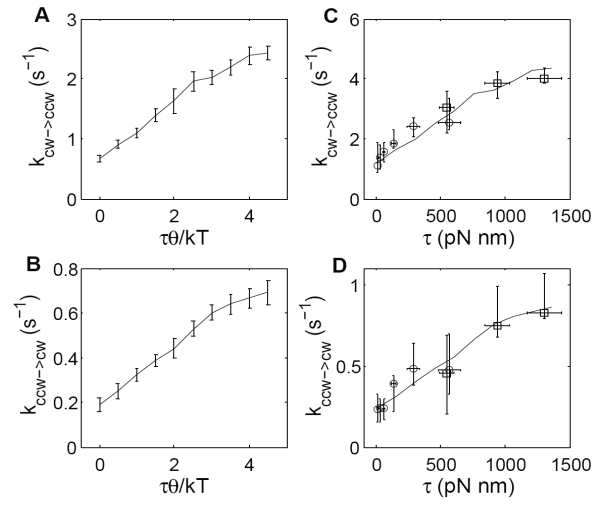


Fig. 9